

Figure 3. Scatter plot of NIRF score versus exergy per faculty ( $X/F$ ).

The Pearson's correlations are also shown in Table 2 and Figures 1–3 show the key relationships between  $X/F$ ,  $X$  and NIRF score as scatter plots. We see that the IITs at Bombay and Kharagpur stand out in terms of research excellence. Another insight is the excellent promise shown by the new IITs at Ropar-Rupnagar and Indore.

We use the bibliometric data that has been released through the NIRF 2016 rankings to see how the top twenty engineering institutions fare if only research excellence is considered as is done in major ranking exercises<sup>1–4</sup>. Unlike the NIRF score, which is one single number, we now decompose performance into a size-dependent exergy term and a size-independent productivity term. We see that the IITs at Bombay and Kharagpur stand out in terms of research excellence. Another insight is the excellent promise shown by the new IITs at Ropar-Rupnagar and Indore.

1. Prathap, G., Benchmarking research performance of the IITs using *Web of Science* and *Scopus* bibliometric databases. *Curr. Sci.*, 2013, **105**, 1134–1138.
2. Bornmann, L., Stefaner, M., de Moya Anegón, F. and Mutz, R., Ranking and mapping of universities and research-focused institutions worldwide based on highly-cited papers: A visualization of results from multi-level models. *Online Inf. Rev.*, 2014, **38**(1), 43–58.
3. Bornmann, L., Stefaner, M., de Moya Anegón, F. and Mutz, R., What is the effect of country-specific characteristics on the research performance of scientific institutions? Using multi-level statistical models to rank and map universities and research-focused institutions worldwide. *J. Inf.*, 2014, **8**(3), 581–593.
4. Bornmann, L., Stefaner, M., de Moya Anegón, F. and Mutz, R., Ranking and mapping of universities and research-focused institutions worldwide: The third release of excellencemapping.net. *COLLNET J. Scientomet. Inf. Manage.*, 2015, **9**(1), 61–68.
5. Katz, J. S., Scale-independent bibliometric indicators. *Measurement*, 2005, **3**(1), 24–28.
6. Prathap, G., The Energy–Exergy–Entropy (or EEE) sequences in bibliometric assessment. *Scientometrics*, 2011, **87**(3), 515–524.

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## Hierarchy of parameters influencing cutting performance of surface miner through artificial intelligence and statistical methods

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**Applicability of a surface miner (SM) must be based on a careful assessment of intact rock and rock mass properties. A detailed literature review was made to identify different parameters influencing the performance of various types of cutting machines deployed in different parts of the world. The critical parameters influencing the production, diesel consumption and pick consumption of SM in Indian coal and limestone mines, were identified through artificial neural network (ANN) technique and screened by correlation coefficient analysis. Parameters that were common in both ANN and correlation analysis were grouped under critical category and others in semi-critical category.**

**Keywords:** Surface miner, intact rock, rock mass, artificial neural network.

INTACT rock, rock mass and machine parameters are broad key parameters that play a key role in cutting performance. Cutting performance is generally evaluated by various parameters such as, production, specific energy, chip size of cut material, cutting force, pick wear, pick consumption, etc. The present study describes an approach to identify critical parameters that affect the performance of SM based on field data collection from various project areas in India. The purpose of identification of the influencing parameters is to understand their relevant importance in the performance of surface miner (SM) and subsequently use them for predicting its performance. Field investigations were conducted in six mines (three each in coal and limestone mines), spread across India representing varied rock mass parameters. The present study conducted under varied rock mass conditions was confined to SM application only. Artificial neural network (ANN) and correlation tools were used to arrive at critical parameters influencing performance of SM in Indian geo-mining conditions with respect to production, diesel consumption and pick consumption.

The following are the intact rock parameters: Rock density: Dry density is a key property that affects specific energy (SE) while cutting<sup>1</sup>. A rock with higher specific gravity or density will need higher SE in cutting. Kahraman

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*et al.*<sup>2</sup> correlated rock density to determine penetration rate of percussive drills. Kirsten<sup>3</sup> identified rock density as an influencing parameter in the excavability assessment of the rock.

**Moisture content:** Moisture content affects the uniaxial compressive strength (UCS) of the rock<sup>4</sup>. Presence of moisture adversely affects mechanical cutting of those materials which turn sticky if wet, like consolidated soil, bentonite, and some types of claystone, shale, marl and siltstone.

**UCS:** Rock strength is one of the most important parameters evaluated in rock mechanics<sup>5</sup>. Evans<sup>6</sup> proposed a cutting theory that used UCS and tensile strength (TS) as input variables for determining cutting and normal force (vertical component of the cutting force). The SM manufacturers follow simple conjecture and use UCS of rocks as the only yardstick to define the cutting ability of their machines or to assess the cutting ability of rocks with respect to any given machine<sup>7</sup>.

**Brazilian tensile strength:** The cutting force estimation model used by Evans<sup>8</sup> for coal, taking TS as the main criteria, found wider acceptance for predicting cutting forces in brittle materials. Thuro<sup>9</sup> took TS as one of the rock properties for predicting drillability. Murthy *et al.*<sup>10</sup> considered TS for cuttability assessment of road header (RH).

**Point load strength index (PLSI):** Point load test is useful for strength classification of intact rocks. Hadjigeorgiu and Scoble<sup>11</sup> developed an excavation index classification scheme by considering PLSI as one of the parameters. Dey and Ghose<sup>12</sup> considered PLSI as one of the key influencing parameters for determination of cuttability of SM.

**Seismic wave velocity:** In the field of rock mechanics, seismic refraction method is the most popular method and is useful in rock mass characterization in surface mines helping in the selection of an excavation system<sup>13</sup>. The measurement of P-wave velocity is a significant way to determine the mechanical parameters of a rock mass<sup>14</sup>.

**Abrasiveness:** More abrasive a rock, more wear and tear it causes on cutting tools of the machine thus affecting its cutting performance adversely. Origliasso *et al.*<sup>15</sup> considered rock abrasivity as one of the key influencing parameters for cuttability determination of SM. Thuro and Plinninger<sup>16</sup> discussed the application of the Cerchar Abrasivity Index (CAI) in the estimation of tool wear rates for hard rock operations. Murthy *et al.*<sup>17</sup> considered CAI as one of the parameters to develop cuttability index of SM.

**Petrography:** Roxborough<sup>18</sup> stressed that rock mineralogy, particularly its quartz content, is often of crucial significance to cutting. Howarth and Rowlands<sup>19</sup> developed a model to predict drillability. This model depends on textural properties of the rock such as grain shape and orientation, degree of grain interlocking, and packing density. According to Tiriyaki and Dikmen<sup>1</sup>, pick forces are expected to increase in linear rock cutting as the texture coefficient increases.

The following are the rock mass parameter: Discontinuities: Presence of joints and other structural features like bedding planes, cleats, slips, etc. in high frequency along with their length and degree of openness assist the cutting process, especially when they are favourably oriented with respect to the direction of cutting. Evans and Pomeroy<sup>20</sup> demonstrated that the orientation of cleats to the direction of cutting can have an important influence on cutter performance with drag picks.

Roxborough and Phillips<sup>21</sup> reported that less SE of about 0.22 MJ/bcm is required when the cutting direction of picks is parallel to coal cleats (cleat orientation = 0°) as shown in Figure 1.

**Rock quality designation (RQD):** Kirsten<sup>3</sup> identified RQD for determining excavability of the rock. Bilgin *et al.*<sup>22</sup> used RQD to estimate the advance rate of a RH. Murthy *et al.*<sup>17</sup> developed a relation between block RQD and production by SM.

**Schmidt rebound hardness number (RN):** Shimada and Matsui<sup>23</sup> used rock impact hardness number for prediction of drivage/drilling rate. Goktan and Gunes<sup>24</sup> determined Schmidt hammer rebound number for predicting cutting rates for a RH. According to Adebayo<sup>25</sup>, RN exhibited a strong correlation with the cutting rate.

**Rock mass rating (RMR):** Many models were developed relating RH performance to rock mass properties such as RMR and RQD values<sup>26</sup>. Bilgin *et al.*<sup>27</sup> utilized UCS, RQD and machine power to predict the instantaneous cutting rate.

Based on the above literature review, it may be summarized that machine cutting performance is influenced significantly by intact rock and rock mass properties (Figure 2). Some of the relations developed by researchers on cutting performance under varied conditions with rock parameters are given in Table 1.

Performance of SM depends on machine configuration such as cutting tool configuration (rake angle, attack angle, clearance angle and tip angle, pick lacing, type of pick, number of picks, tip material), drum weight, drum

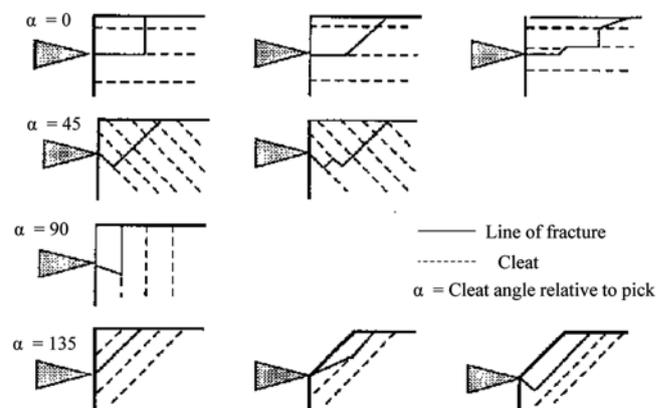


Figure 1. Types of fracture in cleated coals<sup>21</sup>.

**Table 1.** Relations of cutting performance on rock parameters

Rock parameter	Relation	Test condition	Reference
Density	PR = -0.8 ρ + 3.25 (r = 0.60) SE = -68.44 + 33.11ρ (r <sup>2</sup> = 0.74) Wg = 5e <sup>-5PD</sup> + 0.011 for feldspar granite (r <sup>2</sup> = 0.778)	Percussive drill Laboratory Laboratory	Kahraman <i>et al.</i> <sup>2</sup> Tiryaki and Dikmen <sup>1</sup> Adebayo <sup>28</sup>
Moisture content	SE = -2.58lnMC + 13.79 (r <sup>2</sup> = 0.85)	Laboratory	Mammen <i>et al.</i> <sup>29</sup>
UCS	Pr = 1004.9 - 558.73log(σ <sub>c</sub> ) (r <sup>2</sup> = 0.94) ICR = 25.694e <sup>-0.0206σ<sub>c</sub></sup> , RQD > 50 (r <sup>2</sup> = 0.54) ICR = 19.773e <sup>-0.008σ<sub>c</sub></sup> , RQD < 50 (r <sup>2</sup> = 0.19) CR = -0.443σ <sub>c</sub> + 43.97 (r <sup>2</sup> = 0.86) CR = 75.7 - 14.3lnσ <sub>c</sub> (r <sup>2</sup> = 0.62) PR = -0.0079σ <sub>c</sub> + 1.67 (r = 0.97) SE = 3.6 + 0.17σ <sub>c</sub> (r <sup>2</sup> = 0.52) ICR = 444.35σ <sub>c</sub> <sup>-0.8377</sup> (r <sup>2</sup> = 0.29)	SM RH (71 kW) RH (71 kW) RH RH (132 kW) Percussive drill Laboratory Laboratory	Kramadibrata and Shimada <sup>30</sup> Bilgin <i>et al.</i> <sup>27</sup> Bilgin <i>et al.</i> <sup>27</sup> Copur <i>et al.</i> <sup>31</sup> Thuro and Plinninger <sup>32</sup> Kahraman <i>et al.</i> <sup>2</sup> Tiryaki and Dikmen <sup>1</sup> Adebayo <sup>25</sup>
TS	$F_c = \frac{16\pi d^2 \sigma_t^2}{\cos^2(\phi/2)\sigma_c}$ (point attack picks) PR = -0.083σ <sub>t</sub> + 1.68 (r = 0.91) ICR = 67.128σ <sub>t</sub> <sup>-0.6578</sup> (r <sup>2</sup> = 0.65) SE = 0.67 + 3.12σ <sub>t</sub> (r <sup>2</sup> = 0.89)	Laboratory  Percussive drill RH Laboratory	Evans <sup>8</sup>  Kahraman <i>et al.</i> <sup>2</sup> Kelles <sup>33</sup> Tiryaki and Dikmen <sup>1</sup>
PLSI	PR = -0.096I <sub>s</sub> + 1.6 (r = 0.8) SE = 1.28 + 5.06I <sub>s</sub> (r <sup>2</sup> = 0.68) P = 1237.8I <sub>s</sub> <sup>0.308</sup> (r <sup>2</sup> = 0.91)	Percussive drill Laboratory SM	Kahraman <i>et al.</i> <sup>2</sup> Tiryaki and Dikmen <sup>1</sup> Meena <i>et al.</i> <sup>34</sup>
Abrassiveness	CAI = 0.6 + 3.32F CR = -0.528SiO <sub>2</sub> + 50.08 (r <sup>2</sup> = 0.86) Wg = 0.002SiO <sub>2</sub> - 0.126 for feldspar granite (r <sup>2</sup> = 0.83)	Laboratory Laboratory Laboratory	Lislerud <sup>35</sup> Adebayo <sup>25</sup> Adebayo <sup>28</sup>
Petrography	SE = 21.86 - 0.32flds (r <sup>2</sup> = 0.60) SE = 4.27 + 2.21te (r <sup>2</sup> = 0.56)	Laboratory Laboratory	Tiryaki and Dikmen <sup>1</sup> Tiryaki and Dikmen <sup>1</sup>
RQD	RMCI = σ <sub>c</sub> (RQD/100) <sup>2/3</sup> ICR = 50.222RQD <sup>-0.5654</sup> (r <sup>2</sup> = 0.60), σ <sub>c</sub> = 90-100 MPa	RH RH (71 kW)	Bilgin <i>et al.</i> <sup>27</sup> Bilgin <i>et al.</i> <sup>27</sup>
RN	PR = -0.037RN + 1.60 (r <sup>2</sup> = 0.90) CR = -0.6405RN + 43.1 (r <sup>2</sup> = 0.73) SE = -14.1 + 0.68RN (r <sup>2</sup> = 0.79) CR = -0.922RN + 62.62 (r <sup>2</sup> = 0.86)	Percussive drill RH (90 kW) Laboratory Laboratory	Kahraman <i>et al.</i> <sup>2</sup> Goktan and Gunes <sup>24</sup> Tiryaki and Dikmen <sup>1</sup> Adebayo <sup>25</sup>

ρ = Density (g/m<sup>3</sup>); σ<sub>c</sub> = Uniaxial compressive strength (MPa); σ<sub>t</sub> = Brazilian tensile strength (MPa); MC = Moisture content (%); flds = Feldspar (%); SiO<sub>2</sub> = Silica (%); te = Texture coefficient; RN = Rebound hardness number; RQD = Rock quality designation; Is = Point load strength index; PD = Packing density = Summed length of grains measured along traverse/length of traverse (%); SE = Specific energy (MJ/m<sup>3</sup>); Wg = Bit wear rate (mm/m); PR = Penetration rate (m/min); CR = Cutting rate (m<sup>3</sup>/h); ICR = Instantaneous cutting rate (m<sup>3</sup>/h); Pr = Production (bank cm/h); F = Wear index = (QD σ<sub>t</sub>/100), Q = Equivalent quartz (%); D = Mean quartz grain size (mm); RMCI = Rock mass cuttability index.

width (DW), engine power (EP), nature of coolant for tips, etc. Operational conditions of machine play an important role in production. The production capacities of SM depend on face length, depth of cut, machine speed, DW, etc. The various machine parameters influencing production performance are broadly categorized into cutting tool configuration, specifications of cutting drum, EP, project strategy and operational experience as shown in Figure 3.

Literature review is an excellent means to identify and provide base information of parameters influencing the cutting performance of machines. Several mathematical models were developed for different cutting machines to

understand their performance with respect to intact rock and rock mass parameters. The models mainly covered rock cutting by picks, SE, cuttability and production prediction by different machines as shown in Table 2.

Fourteen distinct intact rock, rock mass and machine parameters were identified from literature to assess the cutting performance of mechanical excavators in general. UCS was considered as the most dominant parameter due to its consistency in predicting machine performance and hence, was used by many researchers.

The critical parameters were also identified by ANN technique-based on relative importance and sensitivity. The relative importance and sensitivity are represented by

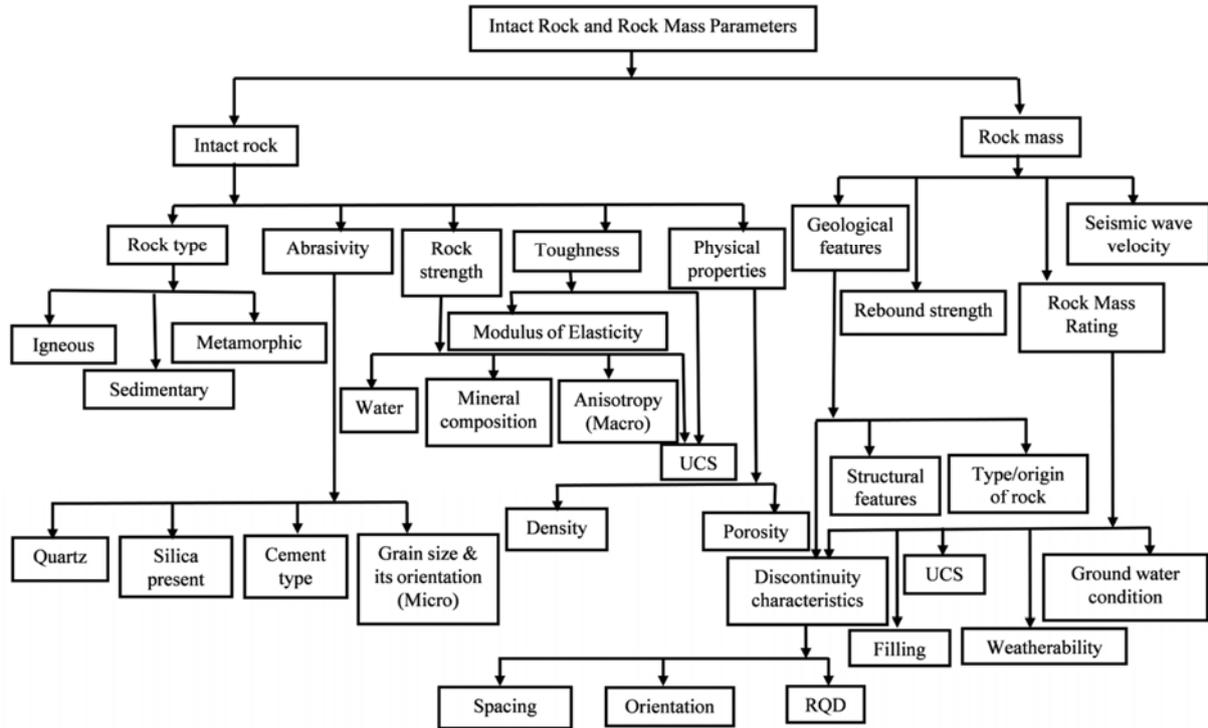


Figure 2. Intact rock and rock mass parameters influencing machine performance.

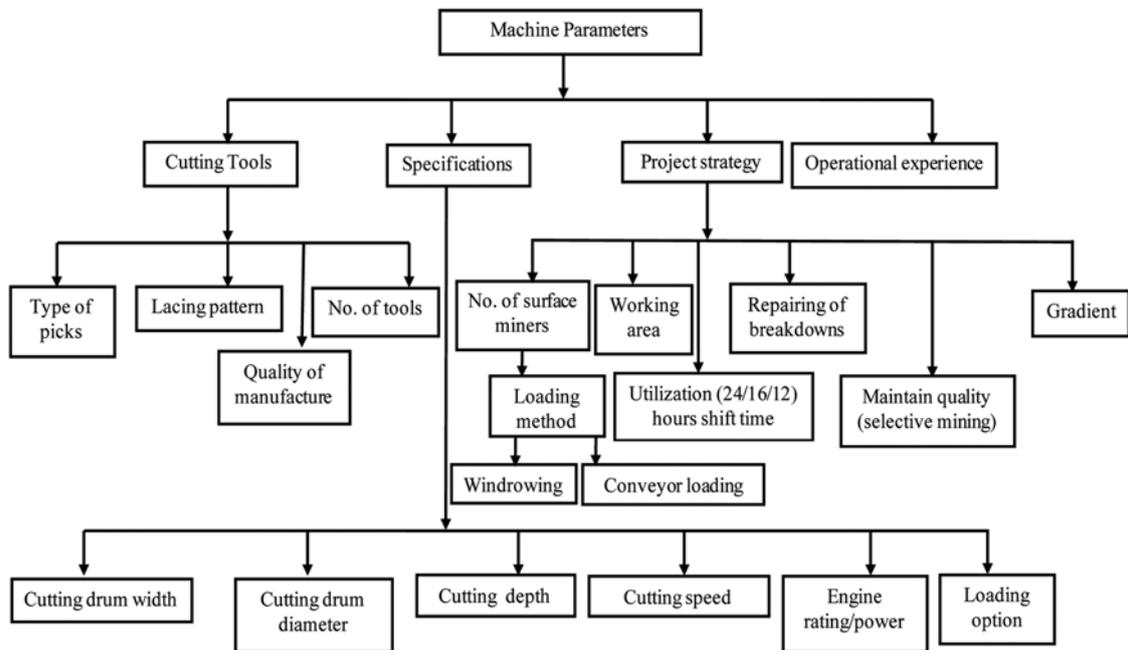


Figure 3. Machine parameters influencing production performance.

weights of different input parameters in the networks. EasyNN software (demo version) was used for analysis. It grows multi-layer neural networks from the data in a grid. The neural network input and output layers are created to match the grid input and output columns. Hidden

layers connecting the input and output layers can then be grown to hold the optimum number of nodes. Each node contains a neuron and its connection addresses.

Neural networks allow the training data to understand the grid and they can use the validating data in the grid to

**Table 2.** Parameters used in empirical relationships for predicting machine performance

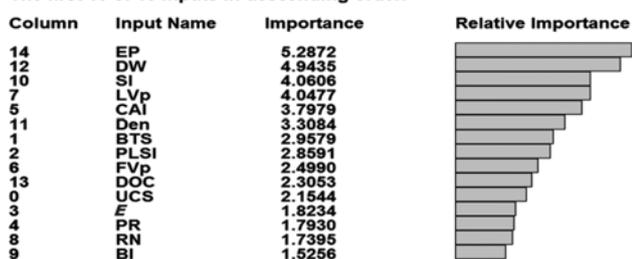
Parameters → Models ↓	1	2	3	4	5	6	7	8	9	10	11	12	13	14
Evans <sup>8</sup>	☐	☐												
Barendsen <sup>36</sup>	☐													
Atkinson <sup>13</sup>								☐						
Franklin <i>et al.</i> <sup>37</sup>									☐					
Kirsten <sup>3</sup>						☐	☐							
Singh <i>et al.</i> <sup>38</sup>	☐									☐				
Farmer <sup>39</sup>	☐									☐				
Roxborough <sup>18</sup>	☐											☐		
Bilgin <i>et al.</i> <sup>22</sup>	☐						☐							
Gehring <sup>40</sup>	☐					☐						☐		☐
Hadjigeorgiu and Scoble <sup>11</sup>					☐				☐					
Jones and Kramadibrata <sup>41</sup>	☐													
Kramadibrata and Shimada <sup>30</sup>	☐	☐	☐			☐				☐	☐	☐		
Tiryaki and Dikmen <sup>1</sup>		☐												
Murthy <i>et al.</i> <sup>17</sup>				☐				☐				☐	☐	☐
Dey and Ghose <sup>42</sup>						☐			☐		☐	☐		
Kahraman <i>et al.</i> <sup>2</sup>			☐											
Total	9	3	2	1	1	4	2	2	3	3	2	5	1	2

1, UCS; 2, TS; 3, Density; 4, Silica percentage (SI); 5, Ground structure/weathering condition; 6, Joints; 7, RQD; 8, Seismic velocity; 9, PLSI; 10, E; 11, Abrasivity; 12, Machine/cutter head power; 13, Machine specifications; 14, Operational condition.

**Table 3.** Critical parameters identified by ANN

Performance Properties	Production (t/h)	Diesel consumption per 1000 t (l)	Pick consumption per 1000 t (nos)
Intact rock and rock mass parameters	<i>In situ</i> P-wave velocity (IV <sub>p</sub> )	RN	Rock density
	Laboratory P-wave velocity (LV <sub>p</sub> )	SI	SI
	CAI	E	UCS
	Rock density	Rock density	E
	SI	LV <sub>p</sub>	Brittleness index (BI)
	TS	IV <sub>p</sub>	TS
Machine parameters	EP	–	Depth of cut
	DW		EP

Untitled 22 cycles. Target error 0.0500 Average training error 0.046474  
The first 15 of 15 Inputs in descending order.



**Figure 4.** Relative importance of parameters with respect to production.

self-validate at the same time. During training, software assigns a weightage to the various inter-related parameters and attempts to limit the error. This process is repeated until the error converges to set limits. The final weightages are obtained after training. After the training

neural networks can be tested using the querying data in the grid, using the interactive query facilities or using querying data in separate files. The values for each parameter were investigated with respect to production, diesel and pick consumption per 1000 t and are shown correspondingly in Figures 4–9.

The top five intact rock and rock mass parameters exclusive of machine parameters based on highest relative importance and sensitivity were identified as critical parameters. The outcome of this analysis is depicted in Table 3. Analysis by ANN being qualitative in nature does not yield any numerical relationship with actual machine performance. Thus, developing mathematical models relating the critical parameters is important for further refining and screening. Hence, regression analysis amongst different parameters was carried out.

The correlation coefficients, between critical intact rock and rock mass parameters and the performance of SM in Indian geo-mining conditions, were determined

**Table 4.** Correlation coefficients relating machine performance with intact rock, rock mass and machine parameters

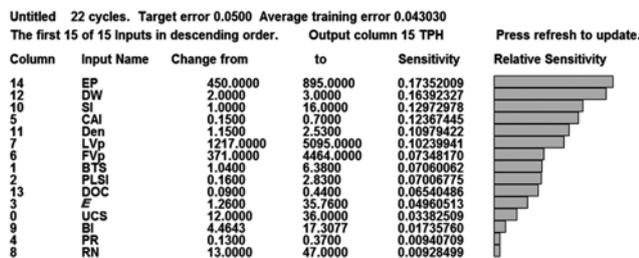
Parameter	$\sigma_c$	$\sigma_t$	$I_s$	E	$\nu$	CAI	$IV_p$	$LV_p$	RN	BI	SI	$\rho$	DW	DOC	EP	TPH	DCT	PCT
$\sigma_c$	1.00	0.79	0.65	0.39	-0.28	0.35	0.01	0.27	-0.18	-0.12	0.12	0.07	-0.09	-0.17	-0.14	-0.12	0.10	-0.07
$\sigma_t$	0.79	1.00	0.67	0.45	-0.37	0.63	0.07	0.40	-0.06	-0.59	0.28	0.12	-0.14	-0.14	-0.14	-0.22	0.24	0.07
$I_s$	0.65	0.67	1.00	0.70	-0.23	0.56	0.34	0.58	-0.47	-0.21	0.52	0.45	-0.10	-0.20	-0.15	-0.27	0.48	0.33
E	0.39	0.45	0.70	1.00	0.04	0.65	0.66	0.90	-0.60	-0.13	0.90	0.84	-0.52	-0.51	-0.56	-0.74	0.88	0.77
$\nu$	-0.28	-0.37	-0.23	0.04	1.00	-0.16	0.13	-0.04	-0.01	0.27	0.17	0.19	-0.01	-0.12	-0.03	0.01	0.07	0.19
CAI	0.35	0.63	0.56	0.65	-0.16	1.00	0.55	0.76	-0.22	-0.38	0.65	0.59	-0.43	-0.41	-0.44	-0.61	0.63	0.46
$IV_p$	0.01	0.07	0.34	0.66	0.13	0.55	1.00	0.80	-0.40	0.08	0.69	0.86	-0.46	-0.59	-0.49	-0.67	0.67	0.60
$LV_p$	0.27	0.40	0.58	0.90	-0.04	0.76	0.80	1.00	-0.57	-0.14	0.87	0.89	-0.56	-0.59	-0.58	-0.81	0.89	0.75
RN	-0.18	-0.06	-0.47	-0.60	-0.01	-0.22	-0.40	-0.57	1.00	-0.30	-0.54	-0.67	0.29	0.49	0.32	-0.48	0.64	0.49
BI	-0.12	-0.59	-0.21	-0.13	0.27	-0.38	0.08	-0.14	-0.30	1.00	-0.18	0.12	-0.08	-0.21	-0.11	-0.02	-0.11	-0.11
SI	0.12	0.28	0.52	0.90	0.17	0.65	0.69	0.87	-0.54	-0.18	1.00	0.83	-0.51	-0.42	-0.52	-0.75	0.94	0.92
$\gamma$	0.07	0.12	0.45	0.84	0.19	0.59	0.86	0.89	-0.67	0.12	0.83	1.00	-0.48	-0.67	-0.51	-0.76	0.86	0.76
DW	-0.09	-0.14	-0.10	-0.52	-0.01	-0.43	-0.46	-0.56	0.29	-0.08	-0.51	-0.48	1.00	0.66	0.99	0.90	-0.59	-0.41
DOC	-0.17	-0.14	-0.20	-0.51	-0.12	-0.41	-0.59	-0.59	0.49	-0.21	-0.42	-0.67	0.66	1.00	0.71	0.71	-0.51	-0.27
EP	-0.14	-0.14	-0.15	-0.56	-0.03	-0.44	-0.49	-0.58	0.32	-0.11	-0.52	-0.51	0.99	0.71	1.00	0.89	-0.59	-0.40
TPH	-0.12	-0.22	-0.27	-0.74	0.01	-0.61	-0.67	-0.81	-0.48	-0.02	-0.75	-0.76	0.90	0.71	0.89	1.00	-0.82	-0.67
DCT	0.10	0.24	0.48	0.88	0.07	0.63	0.67	0.89	0.64	-0.11	0.94	0.86	-0.59	-0.51	-0.59	-0.82	1.00	0.92
PCT	-0.07	0.07	0.33	0.77	0.19	0.46	0.60	0.75	0.49	-0.11	0.92	0.76	-0.41	-0.27	-0.40	-0.67	0.92	1.00

DOC, Depth of cut; TPH, Production in tonnes per hour; DCT, Diesel consumption per 1000t; PCT, Pick consumption per 1000t.

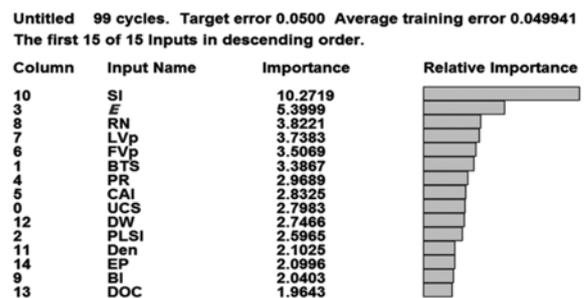
Associative relationship with rock parameters      Associative relationship with PCT.  
 Associative relationship with production      Associative relationship with DCT.

**Table 5.** Critical and semi-critical parameters influencing performance of SM

Performance Criticality	Production (t/h)	Diesel consumption per 1000 t (l)	Pick consumption per 1000 t (nos)
Critical	$IV_p$	RN	Rock density
	$LV_p$	E	E
	Rock density	$LV_p$	SI
	CAI	SI	
	EP	$IV_p$	
	DW		
	SI		
Semi-critical	E	CAI	UCS
	TS	Rock density	TS
			BI
			$LV_p$
			Depth of cut



**Figure 5.** Relative sensitivity of parameters with respect to production.



**Figure 6.** Relative importance of parameters with respect to diesel consumption.

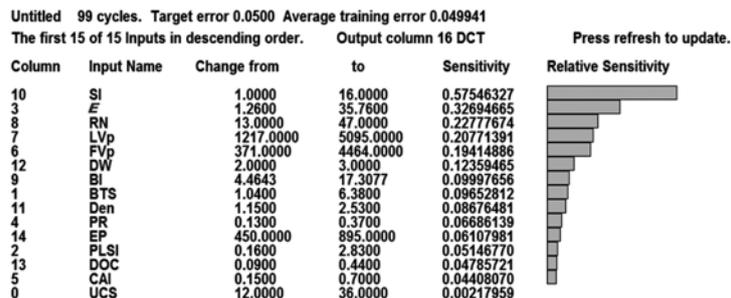


Figure 7. Relative sensitivity of parameters with respect to diesel consumption.

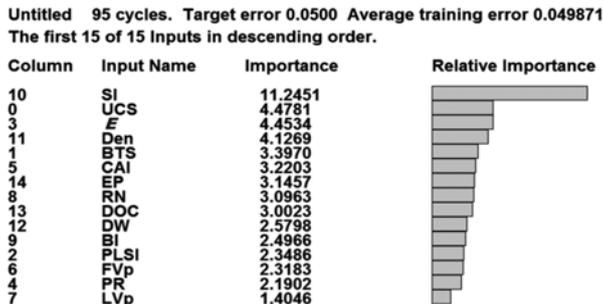


Figure 8. Relative importance of parameters with respect to pick consumption.

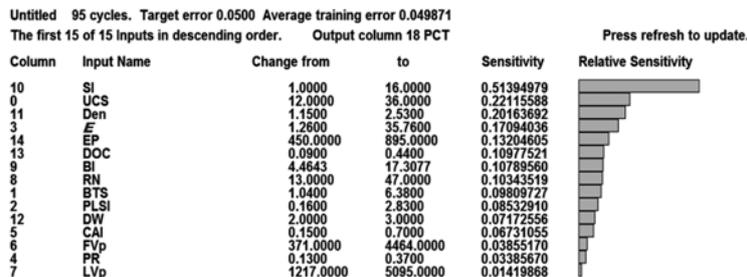


Figure 9. Relative sensitivity of parameters with respect to pick consumption.

(Table 4). The correlation coefficients of different parameters above  $\pm 0.6$  were highlighted in the table with colour codes. Both ANN and correlation analysis have resulted in identifying more or less the same parameters for production, diesel and pick consumption estimation. Parameters that were common in both ANN and correlation analysis were grouped under critical category and others in semi-critical category as given in Table 5.

Parameters that have a bearing on the performance of a cutting machine were initially collated from literature review. Among the identified fourteen distinct intact rock, rock mass and machine parameters, UCS was found to be the most frequently used parameter for assessment of cutting performance of mechanical excavators. ANN analysis was subsequently used to identify the relative importance and sensitivity of different parameters influencing production, diesel and pick consumption of SM for coal and limestone mines of India.

The correlation analysis of each parameter with machine performance further helped in scrutinizing and

screening the parameters into critical and semi-critical categories. All these identified parameters need to be taken into account in the development of acquiescent predictive models of the performance of SM in different rock mass conditions.

1. Tiryaki, B. and Dikmen, A. C., Effects of rock properties on specific cutting energy in linear cutting of sandstones by picks. *Rock Mech. Rock Eng.*, 2006, **39**(2), 89–120.
2. Kahraman, S., Bilgin, N. and Feridunoglu, C., Dominant rock properties affecting the penetration rate of percussive drills. *Int. J. Rock Mech. Min. Sci.*, 2003, **40**, 711–723.
3. Kirsten, H. A. D., A classification system for excavation in natural material. *Civil Eng. S. Afr.*, 1982, 293–307.
4. Fowell, R. J., Johnson, S. T. and Speight, H. E., Assessing the performance of cutting tools in rock materials. In International Symposium on Geotechnical Stability in Surface Mining, Calgary, November 1986, p. 161.
5. Prikryl, R., Some microstructural aspects of strength variation in rocks. *Int. J. Rock Mech. Min. Sci.*, 2001, **38**, 671–682.
6. Evans, I., Basic mechanics of the point attack pick. *Colliery Guardian*, May 1984, pp. 189–193.

7. www.wirtgen.com (accessed on 16 February 2013).
8. Evans, I., The force required for point attack picks. *Int. J. Min. Eng.*, 1965, **2**, 63–71.
9. Thuro, K., Drillability prediction – geological influences in hard rock drill and blast tunnelling. *Geol. Rund.*, 1997, **86**, 426–438.
10. Murthy, V. M. S. R., Munshi, B. and Kumar, B., Predicting roadheader performance from intact rock and rock mass properties – a case study. In Proceedings of National Seminar on Rock–Machine Interaction in Excavations, Banaras Hindu University, Varanasi, 7–8 March 2008, pp. 81–93.
11. Hadjigeorgiu, J. and Scolbe, M. J., Ground characterization for assessment of ease of excavation. In Proceedings of International Seminar on Mine Planning and Equipment Selection (eds Singhal, R. K. and Vavra, M.), Balkema, 1990, pp. 323–331.
12. Dey, K. and Ghose, A. K., Predicting ‘cuttability’ with surface miners – a rockmass classification approach. *J. Mines Met. Fuels*, 2008, **56**(5), 85–92.
13. Atkinson, T., Selection of open pit excavating and loading equipment. *Trans. Inst. Min. Metall. Section A*, 1971, 101–129.
14. Zivor, R., Vilhelm, J., Rudajev, V. and Lokajčiček, T., Measurement of P and S-wave velocities in a rock massif and its use in estimating elastic moduli. *Acta Geod. Geom.*, 2011, **2**(162), 157–167.
15. Origliasso, C., Cardu, M. and Keckojevic, V., Surface miners: evaluation of the production rate and cutting performance based on rock properties and specific energy. *Rock Mech. Rock Eng.*, 2014, **47**, 757–770.
16. Thuro, K. and Plinninger, R. J., Wear prediction in hard rock excavation using the CERCHAR Abrasive Index. In *Rock Engineering – Theory and Practice* (ed. Schubert, W.), 2004, pp. 599–604.
17. Murthy, V. M. S. R., Kumar, D., Jain, P. and Dash, A. K., Development of a cuttability index of surface miner for performance prediction in different geomining conditions. In International Symposium on Rock Mechanics and Geo-Environment in Mining and Allied Industries, Banaras Hindu University, Varanasi, 12–14 February 2009, pp. 156–171.
18. Roxborough, F. F., The role of some basic rock properties in assessing cuttability. In Proceedings of the Seminar on Tunnels, Wholly Engineered Structures, I. E. Aust./AFCC, Sydney, Australia, April 1987, p. 122.
19. Howarth, D. F. and Rowlands, J. C., Development of an index to quantify rock texture for qualitative assessment of intact rock properties. *Geo. Test J.*, 1986, **9**, 169–179.
20. Evans, I. and Pomeroy, C. D., *The Strength, Fracture and Workability of Coal*, Oxford Pergamon Press, Library of Congress Catalog Card No. 66-14657, 1966.
21. Roxborough, F. F. and Phillips, H. R., Applied rock and coal cutting mechanics. Australian Foundation Workshop Course 156/81, 1981.
22. Bilgin, N., Seyrek, T. and Shahria, K., Golden horn clean up contributes valuable data. *Tunn. Tunn.*, 1988, 41–44.
23. Shimada, H. F. and Matsui, K., Prediction of drivage/drilling rate by using rock impact hardness number. In Proceedings of New Horizon in Resource Handling and Geo-Engineering (MMIJ/AusIMM Joint Symposium), Ube, Japan, October 1994, pp. 485–492.
24. Goktan, R. M. and Guneş, N., A comparative study of Schmidt hammer testing procedure with reference to rock cutting. *Int. J. Rock Mech. Min. Sci.*, 2005, **42**, 466–472.
25. Adebayo, B., Evaluation of cuttability of selected rocks in South-Western Nigeria. *Aust. J. Tech.*, 2008, **12**(2), 126–129.
26. Fowell, R. J. and Johnson, S. T., Rock classification and assessment for rapid excavation. In *Strata Mechanics – Developments in Geotechnical Engineering* (ed. Farmer, I. W.), Elsevier Scientific Publishing Company: Amsterdam, 1982, vol. 32, pp. 241–244.
27. Bilgin, N., Yazici, S. and Eskikaya, S., A model to predict the performance of roadheaders and impact hammers in tunnel drivages. In Proceedings of the Eurock 1996 on Prediction and Performance in Rock Mechanics and Rock Engineering (ed. Barla, G.), Balkema, Rotterdam, 1996, vol. 2, pp. 715–720.
28. Adebayo, B., Effect of textural characteristics of rock on bit wear. *Aust. J. Tech.*, 2011, **14**(4), 299–307.
29. Mammen, J., Saydam, S. and Hagan, P., A study on the effect of moisture content on rock cutting performance. In Coal Operators’ Conference (ed. Aziz, N.), University of Wollongong and The Aus Inst Min Metall, Illawarra Branch, Australia, 12–13 February 2009, pp. 340–347.
30. Kramadibrata, S. and Shimada, H., The influence of rock mass and intact rock properties on the design of surface mines with particular reference to the excavation of rock, Part-I, II and III. School of Civil Engineering, Curtin University of Technology, 1996.
31. Copur, H., Ozdemir, L. and Rostami, J., Roadheader application in mining and tunnelling industries. *Min. Eng.*, 1998, 38–42.
32. Thuro, K. and Plinninger, R. J., Roadheader excavation performance – geological and geotechnical influences. In Ninth ISRM Congress Paris, Theme 3: Rock dynamics and tectonophysics/Rock cutting and drilling, 25–28 August 1999.
33. Kelles, S., Cutting performance assessment of a medium weight roadheader at Cayirhan coal mine. Master of Science Thesis, Department of Mining Engineering, The Graduate School of Natural and Applied Science, Middle East Technical University, 2005, p. 58.
34. Meena, P., Kumar, M., Jain, P. and Murthy, V. M. S. R., Performance analysis of surface miner in Indian coal mines – a case study. In Conference on Emerging Trends in Mining and Allied Industries, NIT, Rourkela, 2–3 February 2008, pp. 57–65.
35. Lislrud, A., Principles of mechanical excavation. Posiva 97–12, commissioned by Posiva Oy, Mikonkatu 15 A, FIN 00100 Helsinki, Finland, 1997, p. 244.
36. Barendsen, P., Tunneling with machine working on the undercutting principle. In Proceedings of South African Tunneling Conference (ed. Goodman, J. A.), The Technology and Potential of Tunnelling, 1970, pp. 53–58.
37. Franklin, J. A., Broch, E. and Walton, G., Logging the mechanical character of rock. *Trans. Inst. Min. Metall. Section A*, 1971, 1–9.
38. Singh, R. N., Denby, B., Egretli, I. and Pathon, A. G., Assessment of ground rippability in opencast mining operations. Mining Departmental Magazine, University of Nottingham, 1986, **38**, 21–34.
39. Farmer, I. W., Energy based rock characterization. In Proceedings of International Symposium on Application of Rock Characterization Techniques in Mine Design (ed. Karamis, M.), AIME, Littleton, USA, 1986, pp. 17–23.
40. Gehring, K. H., A cutting comparisons. *Tunn. Tunn.*, 1989, 27–30.
41. Jones, I. O. and Kramadibrata, S., An excavating power model for continuous surface miner. *Aust. Inst. Min. Metall.*, 1995, 17.
42. Dey, K. and Ghose, A. K., Selecting a surface miner – an algorithm. Mining Industry Annual Review for 2009. *J. Mines, Met. Fuels*, 2009, **57**(9), 282–286.

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